

# Development of New Oxygen Ion Conductors Based on $\text{Nd}_4\text{GeO}_8$ and $\text{Nd}_3\text{GaO}_6$

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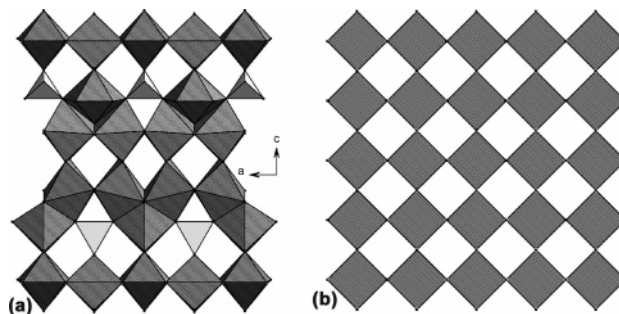
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New oxygen ion conductors have been prepared by substituting  $\text{Ga}^{3+}$  for  $\text{Ge}^{4+}$  in  $\text{Nd}_4\text{GeO}_8$ ,  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  for  $\text{Ga}^{3+}$  in  $\text{Nd}_3\text{GaO}_6$ , and  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  for  $\text{Nd}^{3+}$  in  $\text{Nd}_3\text{GaO}_6$ . A combustion technique using ethylenediamine tetraacetic acid has been developed to synthesize these materials at  $\sim 900^\circ\text{C}$ , leading to powders with spherical particles of about 100–200 nm. The green pellets obtained through the combustion-synthesized powders could be sintered to  $\sim 98\%$  at  $1250^\circ\text{C}$ . It was found that  $\text{Nd}_4\text{Ge}_{1-x}\text{Ga}_x\text{O}_{8-x/2}$  are formed up to  $x = 0.10$ ,  $\text{Nd}_3\text{Ga}_{1-x}\text{M}_x\text{O}_{6-x/2}$  ( $\text{M} = \text{Zn}, \text{Mg}$ ) up to  $x = 0.03$ , and  $\text{Nd}_{3(1-x)}\text{M}'_{3x}\text{GaO}_{6-3x/2}$  up to  $x = 0.03$  and  $0.015$  for  $\text{M}' = \text{Ca}$  and  $\text{Sr}$ , respectively. These relatively small substitution rates induce a significant increase in oxygen ion conductivity ( $\sigma_{800^\circ\text{C}} = 0.2 \times 10^{-2} \text{ S cm}^{-1}$  for  $\text{Nd}_4\text{Ge}_{0.9}\text{Ga}_{0.1}\text{O}_{7.95}$ ;  $\sigma_{800^\circ\text{C}} = 0.5 \times 10^{-2}$  and  $0.4 \times 10^{-2} \text{ S cm}^{-1}$  for  $\text{Nd}_3\text{Ga}_{0.97}\text{M}_{0.03}\text{O}_{5.985}$  with  $\text{M} = \text{Zn}$  and  $\text{Mg}$ , respectively, and  $\sigma_{800^\circ\text{C}} = 0.6 \times 10^{-2}$  and  $0.7 \times 10^{-2} \text{ S cm}^{-1}$  for  $\text{Nd}_{2.91}\text{Ca}_{0.09}\text{GaO}_{5.955}$  and  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$ , respectively) with respect to pure  $\text{Nd}_4\text{GeO}_8$  ( $\sigma_{800^\circ\text{C}} = 2.8 \times 10^{-4} \text{ S cm}^{-1}$ ) and pure  $\text{Nd}_3\text{GaO}_6$  ( $\sigma_{800^\circ\text{C}} = 2.7 \times 10^{-4} \text{ S cm}^{-1}$ ).

## 1. Introduction

In the present solid oxide fuel cells (SOFCs) the favored electrolyte is yttria-stabilized zirconia (YSZ), which exhibits high oxygen ion conductivity at rather high temperature ( $\geq 800^\circ\text{C}$ ). As a consequence, the operating temperature of YSZ-based SOFCs must be high (850–1000  $^\circ\text{C}$ ), and although there are advantages to operating at high temperature, this does induce severe restrictions upon the materials that can be used reliably due to problems associated with thermal cycling and performance degradation that results from increased reactivity of the individual components at higher temperatures. Therefore, there is a great deal of interest in the development of new materials with improved properties that could enable lower-temperature operation.

Since the discovery of fast oxygen ion conduction in YSZ, fluorite-like compounds have been extensively investigated and metal substitution with lower valent cations to form or increase charge-compensating oxygen vacancies has become one of the most common approaches to enhancing oxygen ion conductivity. As part of these continuing efforts to find new electrolyte materials, the principle mentioned above has been applied to  $\text{Nd}_4\text{GeO}_8$ <sup>1</sup> and  $\text{Nd}_3\text{GaO}_6$ .<sup>2,3</sup>



**Figure 1.** [010] view of (a) a fragment of the  $\text{Nd}_4\text{O}_4\text{GeO}_4$  structure and (b) the cubic fluorite structure.

$\text{Nd}_4\text{GeO}_8$  is a neodymium oxy-monogermanate that is better formulated as  $\text{Nd}_4\text{O}_4\text{GeO}_4$ . Its structure [space group (SG)  $Pmc2_1$  with  $a = 7.475(2) \text{ \AA}$ ,  $b = 5.727(2) \text{ \AA}$ , and  $c = 17.927(5) \text{ \AA}$ ] is built up from six kinds of edge-sharing  $\text{NdO}_7$  polyhedra forming a three-dimensional framework to which  $\text{GeO}_4$  tetrahedra are bonded via vertexes (Figure 1a). Inclusion of one next-neighbor oxygen atom in the coordination sphere of each Nd atom enables the structure of  $\text{Nd}_4\text{O}_4\text{GeO}_4$  to be considered as consisting of  $\text{NdO}_8$  distorted cubes and a fluorite-like packing of O atoms to be recognized (Figure 1b).<sup>1</sup> This structural feature prompted us to investigate the possibility of creating oxide ion vacancies by substitution of  $\text{Ga}^{3+}$  for  $\text{Ge}^{4+}$ , to evaluate the potential of the oxygen-deficient compounds as solid electrolytes. Attempts to substitute alkali-earth cations for  $\text{Nd}^{3+}$  resulted in new phases which are presently being identified.

$\text{Nd}_3\text{GaO}_6$  is a neodymium oxy-monogallate whose chemical formula can be better written as  $\text{Nd}_3\text{O}_2\text{GaO}_4$ . Its structure<sup>3</sup> (SG  $Cmc2_1$  with  $a = 9.1820(1) \text{ \AA}$ ,  $b = 11.5396(1) \text{ \AA}$ ,  $c = 5.5748(1) \text{ \AA}$ ) is built up from two kinds of edge-sharing

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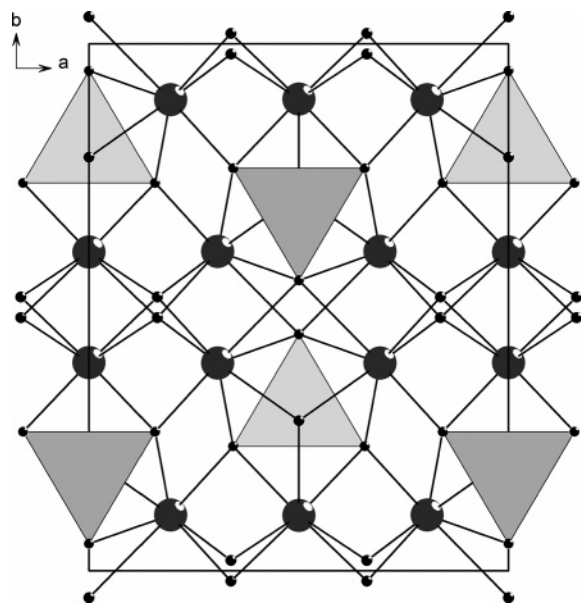
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**Figure 2.** [001] view of the  $\text{Nd}_3\text{O}_2\text{GaO}_4$  structure showing  $\text{GaO}_4$  tetrahedra, Nd (large black circles), and O atoms (small black circles).

$\text{NdO}_7$  polyhedra forming a three-dimensional framework to which  $\text{GaO}_4$  tetrahedra are bonded via vertexes (Figure 2). As in the case of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ , formation of vacancies on oxygen sites coordinated to  $\text{Nd}^{3+}$  cations only can be expected as a result of the large coordination number of neodymium. Therefore, attempts to create oxygen vacancies were made and the potential of the oxygen-deficient phases as solid electrolytes was evaluated.

In solid-state synthesis of compounds with small substitution rates, the major problems are local stoichiometric variations and the requirement of a high calcination temperature which leads to bigger particle size and poor sinterability of the powders. These problems can be overcome to some extent by applying tedious and time-consuming repeated grinding and calcinations steps. A variety of wet-chemical processes have been developed to deal with the shortcomings of solid-state synthesis. However, most of them suffer from disadvantages such as use of expensive and moisture-sensitive metal alkoxides in the case of sol-gel, repeated washing in the case of coprecipitation, and so forth. In addition, in most cases, the end product consists of hard agglomerates which require a post-milling step.

In recent years, the combustion technique has attracted a considerable attention because of its capability to deliver phase-pure, ultrafine powders at low calcination temperature which can be readily sintered to high density at a comparatively lower temperature.<sup>4,5</sup> The technique involves an exothermic decomposition of a homogeneous fuel-oxidant precursor (mostly in the form of a gel) that results in either finely divided powder of the required phase or semi-decomposed precursors containing considerable carbonaceous residue, depending on the nature and amount of fuel used in the process.<sup>6,7</sup> The success of the process is attributed to an atomistic level blending among the constituents, achieved

by using a suitable complexing agent [e.g., citric acid, ethylenediamine tetraacetic acid (EDTA), urea, glycine, etc.] and an exothermic redox reaction between the fuel and an oxidizer (i.e., nitrates). Urea, glycine, and citric acid are the common fuels used in the combustion technique, whereas a few papers report the use of EDTA as a fuel in the combustion technique. However, the versatile ability of EDTA as a complexing agent for a variety of metal ions is well-known. It enables a transparent viscous gel to be obtained by preventing selective precipitation. Furthermore, it can combust with nitrates at low ignition temperature also and, hence, is a good choice as a fuel for the combustion process.

The present paper reports the development of new oxygen ion conductors based on substitutions of  $\text{Ga}^{3+}$  for  $\text{Ge}^{4+}$  in  $\text{Nd}_4\text{O}_4\text{GeO}_4$ ,  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  for  $\text{Ga}^{3+}$  in  $\text{Nd}_3\text{O}_2\text{GaO}_4$ , and  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  for  $\text{Nd}^{3+}$  in  $\text{Nd}_3\text{O}_2\text{GaO}_4$ , using the newly developed EDTA-nitrate combustion process and their characterization in terms of phase purity, grain size, sinterability, and anionic conductivity.

## 2. Experimental Section

All materials used were of analytical reagent grade. Initially, attempts have been made to synthesize  $\text{Nd}_4\text{O}_4\text{GeO}_4$ -based and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials through the conventional solid-state reaction (the terms " $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials" are used throughout the manuscript for both pure and substituted  $\text{Nd}_4\text{O}_4\text{GeO}_4$  and  $\text{Nd}_3\text{O}_2\text{GaO}_4$  phases). The weighed quantities of corresponding oxides were mixed in an agate mortar, ground in acetone, and calcined at  $1200^\circ\text{C}$  for 24 h. The calcined powders of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials were ground, made into pellets, and fired at  $1400$  and  $1250^\circ\text{C}$ , respectively, for 72 h.

For the synthesis of  $\text{Nd}_4\text{O}_4\text{GeO}_4$  and  $\text{Nd}_3\text{O}_2\text{GaO}_4$  through the EDTA-nitrate combustion technique, separate aqueous solutions of metal nitrates and EDTA were prepared. Neodymium nitrate solution was prepared by dissolving  $\text{Nd}_2\text{O}_3$  in a minimum volume of dilute  $\text{HNO}_3$ . Because  $\text{GeO}_2$  is not soluble in an acidic medium, it was first dissolved in a minimum volume of dilute aqueous ammonia. The complex formed is soluble in a nitric medium. The aqueous solution of gallium nitrate was prepared from  $\text{Ga}(\text{NO}_3)_3 \cdot x\text{H}_2\text{O}$ . Prior to its use, the exact composition of this latter material was analyzed by performing thermogravimetric analysis (TGA). The EDTA ( $\text{C}_{10}\text{H}_{16}\text{N}_2\text{O}_8$ ) solution was prepared by dissolving its required quantity in a minimum volume of dilute aqueous ammonia. The solutions of metal nitrates and EDTA were mixed together in the required molar ratio to obtain transparent metal nitrate-EDTA solutions. The molar ratio of total metal ions to EDTA was maintained at 1:0.5.

As an example, the metal nitrate-EDTA solution that was used for the synthesis of  $2 \times 10^{-3}$  mol (1.553 g) of  $\text{Nd}_4\text{Ge}_{0.9}\text{Ga}_{0.1}\text{O}_{7.95}$  was prepared as follows: 1.3459 g ( $4 \times 10^{-3}$  mol) of  $\text{Nd}_2\text{O}_3$  was dissolved at  $\sim 80^\circ\text{C}$  in 40 mL of a 0.785 M solution of  $\text{HNO}_3$  (i.e., with an excess of  $\sim 30\%$  in  $\text{HNO}_3$  with respect to the formation of  $\text{Nd}^{3+}$  nitrate, to ensure complete and rather fast dissolution of the oxide) and 20 mL of a  $10^{-2}$  M aqueous solution of  $\text{Ga}(\text{NO}_3)_3 \cdot x\text{H}_2\text{O}$  was added to this  $\text{Nd}^{3+}$  solution. Then, 0.1883 g ( $1.8 \times 10^{-3}$  mol) of  $\text{GeO}_2$  was dissolved at  $\sim 80^\circ\text{C}$  in 24 mL of an aqueous 1 M solution of ammonia, and this solution was poured slowly into

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the beaker containing the  $\text{Nd}^{3+}/\text{Ga}^{3+}$  solution under continuous stirring. The EDTA solution was prepared by dissolving 1.4612 g ( $5 \times 10^{-3}$  mol) of the solid in 10 mL of an aqueous 1 M solution of ammonia. It was added to the metal nitrate solution under stirring.

The thermal dehydration of metal nitrate–EDTA solutions (at  $\sim 100$  °C on a hot plate) resulted in a highly viscous gel. As soon as the gel is formed, the temperature of the hot plate was increased to  $\sim 300$  °C. At this stage, the gel swelled and auto-ignited in a controlled and self-sustaining manner with the evolution of a large volume of gases to produce voluminous blackish powder hereafter termed as the precursor. The  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  substituted compounds were prepared in a similar way using  $\text{Zn}(\text{CH}_3\text{COO})_2 \cdot x\text{H}_2\text{O}$  and  $\text{Mg}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$  as their corresponding raw materials. The exact amount of water in these materials was determined by TGA before their use. Calcium and strontium nitrate solutions were prepared by decomposition of the corresponding carbonates in a minimum volume of dilute  $\text{HNO}_3$ .

The precursors obtained after auto-ignition were calcined at various temperatures to remove the carbonaceous residues and to determine phase evolution. X-ray diffraction (XRD) patterns of the combustion-synthesized powders were recorded on a Siemens D5000 diffractometer using  $\text{Cu K}\alpha$  radiation.

The combustion synthesized powders of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials were ground in acetone for 5 min using a pestle and mortar and then cold-pressed in the form of 10-mm-diameter pellets at a pressure of 1 kbar using a uniaxial hydraulic press. Stearic acid was used as a lubricant. Sintering was performed in air at 1250 °C for 4 h at a 10 °C/min heating rate.

The XRD patterns of the sintered samples were recorded at room temperature using an INEL position-sensitive detector ( $\text{Cu K}\alpha$ :  $\lambda = 1.540598$  Å). Refinements of cell parameters were carried out using the program FULLPROF<sup>8</sup> in the full pattern matching mode, and its interface is the program WinPLOTR.<sup>9</sup>

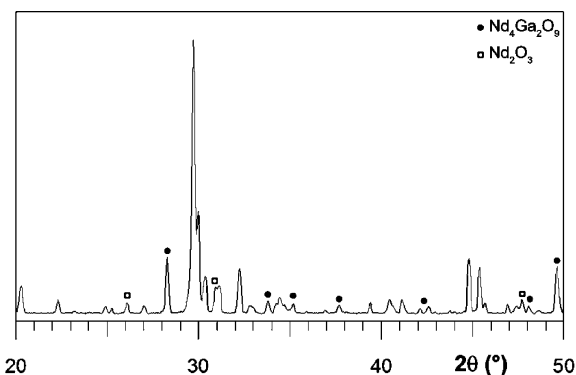
Densities of sintered materials were determined by measuring the dimensions and weight of the pellets. The morphology and microstructure studies on combustion-synthesized powders and sintered pellets were carried out using a JEOL JSM 6400F scanning electron microscope. Energy-dispersive X-ray (EDX) analyses were systematically performed on numerous single crystals with a Link System OXFORD analyzer.

Conductivity measurements were made with the use of samples in the form of pellets using a model 1260 high-frequency response analyzer of M/s Solartron (Schlumberger, U.K.) with a 500 mV of alternating current (ac) perturbation, from 0.01 Hz to 2 MHz, between 250 and 800 °C, in dry air. Both sides of the pellets were coated with Pt paste acting as electrodes. Some measurements were also made under reduced oxygen partial pressures [ $10^{-5}$  atm using  $\text{N}_2$  from the laboratory network, and  $10^{-20}$  atm with an  $\text{Ar-H}_2$  (5%) gas mixture] which were measured with the use of a YSZ-based oxygen sensor placed next to the pellet. The complex impedance spectra were analyzed with Zview (Scribner Associates, Inc.) and MicW<sup>10</sup> electrochemical impedance softwares.

### 3. Results and Discussion

#### 3.1. Investigation of Synthesis and Sintering Conditions.

When  $\text{Nd}_4\text{O}_4\text{GeO}_4$  materials were prepared by solid-state reaction and sintered at 1400 °C, the pellet densities were



**Figure 3.** Synthesis of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  by solid-state reaction: XRD pattern of a sample heated at 1250 °C for 72 h, showing  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$  as impurity phases along with  $\text{Nd}_3\text{O}_2\text{GaO}_4$  as a major phase.

found to be 80%, which is too low for accurate measurements of the ionic conductivity.

Initial attempts to synthesize  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials through conventional solid-state reaction were not successful as result of the easy formation of the stable intermediate cuspidine type compound  $\text{Nd}_4\text{Ga}_2\text{O}_9$ .<sup>11</sup> Figure 3 shows the XRD pattern of the sample calcined at 1250 °C for 72 h, which reveals  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$  as impurity phases along with  $\text{Nd}_3\text{O}_2\text{GaO}_4$  as a major phase. Rao et al.<sup>3</sup> also faced the same problem during the synthesis of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  through solid-state reaction.

Because phase purity, homogeneous distribution of substituents, and well-sintered samples affect the conducting characteristics significantly, attempts have been made to synthesize  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials through the newly developed EDTA–nitrate combustion technique. Generally, the amount of fuel used in the combustion process is decided by using the principle of propellant chemistry,<sup>12</sup> according to which, for a stoichiometric combustion reaction, the coefficient of total oxidizing valency of metal nitrate to total reducing valency of fuel should be unity.

To prepare powder in a somewhat larger quantity without leaving any flame/fire and powder outside the beaker, controlling the combustion reaction is an equally important aspect of the process. Fuel-deficient and stoichiometric combustion reactions are normally highly exothermic and, hence, difficult to control.<sup>4,13</sup> To control the combustion kinetics, a fuel-rich composition was used.<sup>3,4</sup> Hence, a large excess of EDTA was used to control the combustion reactions for the synthesis of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials. The combustion reactions were found to occur in a self-sustaining and controlled manner when a total metal ions to EDTA molar ratio of 1:0.5 was used. However, the products contained considerable amount of carbonaceous residues and were amorphous in nature as indicated by the XRD pattern of the as-prepared powder obtained during the

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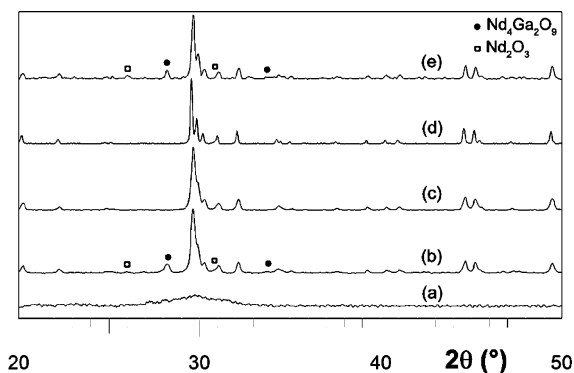
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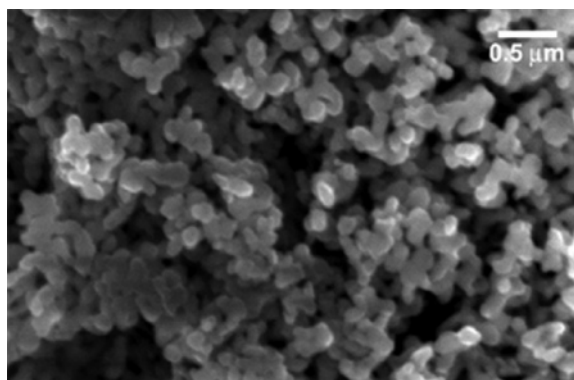
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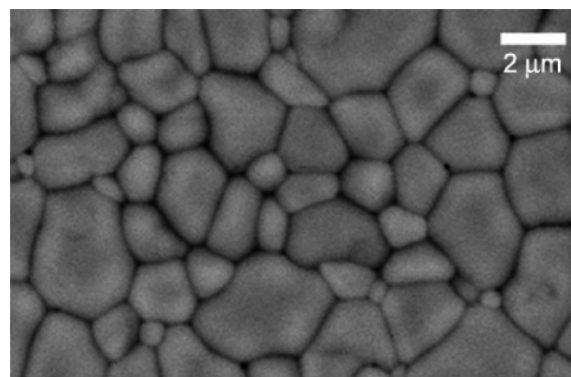


**Figure 4.** XRD pattern of (a) as-prepared powder obtained during the combustion synthesis of  $\text{Nd}_3\text{O}_2\text{GaO}_4$ , (b) as-prepared powder plus calcination at  $800\text{ }^\circ\text{C}$  for 4 h (showing trace amounts of  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$ ), (c) as-prepared powder plus calcination at  $900\text{ }^\circ\text{C}$  for 4 h, (d) as-prepared powder plus pelletization and sintering at  $1250\text{ }^\circ\text{C}$  for 4 h, and (e) as-prepared powder plus calcination at  $1350\text{ }^\circ\text{C}$  for 12 h (showing trace amounts of decomposition products  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$ ).



**Figure 5.** SEM micrograph of a  $\text{Nd}_3\text{O}_2\text{GaO}_4$  sample prepared by the combustion technique (see text) and further calcined at  $900\text{ }^\circ\text{C}$  for 4 h.

combustion synthesis of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  (Figure 4a). Similar XRD patterns were observed for all  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials. The as-prepared powders were calcined at different temperatures to determine the minimum temperature required for phase formation. The XRD pattern of the powder calcined at  $800\text{ }^\circ\text{C}$  for 4 h (Figure 4b) reveals the presence of a small amount of impurity phases of  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$ . However, the pure  $\text{Nd}_3\text{O}_2\text{GaO}_4$  phase was obtained when the powder was calcined at  $900\text{ }^\circ\text{C}$  for 4 h as indicated by the XRD pattern given in Figure 4c. The XRD data suggest that, despite the formation of a small amount of impurities, as in the case of solid-state synthesis, phase pure material can be obtained at temperatures as low as  $900\text{ }^\circ\text{C}$  probably due to the high reactivity of the combustion-synthesized  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$ . XRD patterns of  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  substituted  $\text{Nd}_3\text{O}_2\text{GaO}_4$  have also reflected the same kind of behavior. The  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials obtained at  $900\text{ }^\circ\text{C}$  were used for sintering. Scanning electron microscopy (SEM) micrographs of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  powder obtained at  $900\text{ }^\circ\text{C}$  shows it to consist of spherical particles of about  $100\text{--}200\text{ nm}$  (Figure 5). The agglomerates seem to be soft in nature and having low strength. High surface energy associated with ultrafine particles is responsible for agglomeration through weak van der Waals forces. No significant partial sintering among particles was observed. The powder seems to be suitable for low-temperature sintering. The SEM observations on all



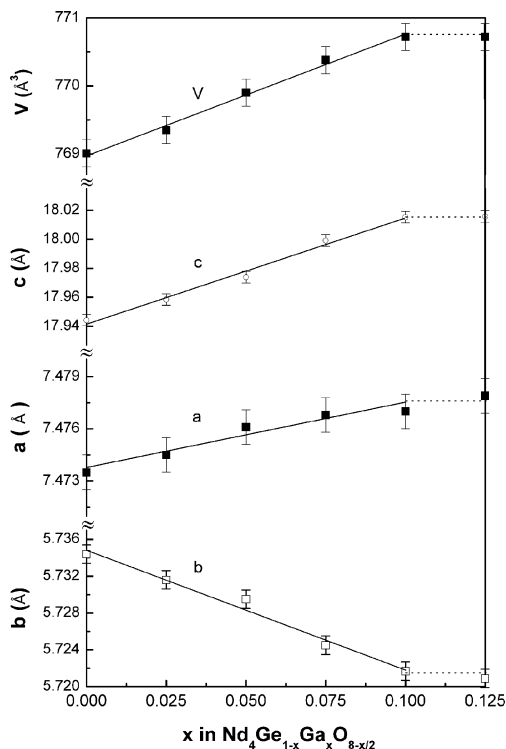
**Figure 6.** SEM micrograph of a fracture surface of a dense pellet of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  sintered at  $1250\text{ }^\circ\text{C}$  for 4 h.

$\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials have also reflected the same kind of morphology of the powders.

The  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials sintered at  $1250\text{ }^\circ\text{C}$  for 4 h exhibit a density  $\sim 98\%$  of the theoretical. Under such conditions, the pure  $\text{Nd}_3\text{O}_2\text{GaO}_4$  phase was obtained as indicated by the XRD pattern given in Figure 4d. The SEM micrograph of  $\text{Nd}_3\text{Ga}_{0.97}\text{Zn}_{0.03}\text{O}_{5.985}$  sintered  $1250\text{ }^\circ\text{C}$  for 4 h (Figure 6) reflects the dense microstructure with grain size of about  $0.5\text{--}4.0\text{ }\mu\text{m}$ . Similar observations were made on  $\text{Nd}_4\text{O}_4\text{GeO}_4$ -based samples whereas  $\text{Nd}_3\text{O}_2\text{GaO}_4$  and  $\text{Mg}^{2+}$  doped sintered samples exhibited a smaller grain size. The densification of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials at such a low temperature and without any post-milling step was achieved because of the ultrafine nature of the starting powder associated with high surface area and absence of hard agglomeration among particles. It is important to note that  $\text{Nd}_3\text{O}_2\text{GaO}_4$  is not stable above  $1300\text{ }^\circ\text{C}$ .<sup>2</sup> Figure 4e shows the XRD pattern of the powder calcined at  $1350\text{ }^\circ\text{C}$  for 12 h, which suggests decomposition of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  to form  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$ .

All samples were further analyzed for their cation content by EDX on grains chosen in different areas. For  $\text{Nd}_3\text{O}_2\text{GaO}_4$ ,  $\text{Nd}_4\text{O}_4\text{GeO}_4$ , and  $\text{Nd}_4\text{O}_{4-x/2}\text{Ge}_{1-x}\text{Ga}_x\text{O}_4$  materials with  $x \geq 0.05$ , these elemental analyses gave nominal formulas in very good agreement with the starting compositions. For all other compositions corresponding to smaller substitution rates, the EDX technique is not sensitive enough to analyze the concentration of dopants accurately. However, these dopants were detected and SEM backscattering electron images of samples upon sintering at high temperature were indicative of compositional homogeneity.

**3.2. Structural Studies.** (a)  $\text{Nd}_4\text{O}_{4-x/2}\text{Ge}_{1-x}\text{Ga}_x\text{O}_4$  ( $x < 0.125$ ). Analysis of XRD patterns recorded for compounds with  $x \leq 0.125$  showed that solid solutions are formed up to  $x = 0.1$ . For  $x = 0.125$ , diffraction peaks are shifted slightly further with respect to  $x = 0.1$  and weak extra peaks corresponding to trace amounts of  $\text{Nd}_4\text{Ga}_2\text{O}_9$  and  $\text{Nd}_2\text{O}_3$  were observed, indicating that the limit of the solid solution is situated between these two latter compositions. Figure 7 illustrates the evolution of the orthorhombic cell parameters with Ga content. As expected, replacement of  $\text{Ge}^{4+}$  (effective ionic radii in 4-fold coordination:  $r_e^{(IV)} = 0.39\text{ \AA}$ )<sup>14</sup> by  $\text{Ga}^{3+}$



**Figure 7.** Evolution of cell parameters and cell volume with the Ga content in  $\text{Nd}_4\text{O}_{4-x/2}\square_{x/2}(\text{Ge}_{1-x}\text{Ga}_x\text{O}_4)$  compounds.

**Table 1.** Cell Parameters of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  and  $\text{Nd}_3\text{Ga}_{0.97}\text{M}_{0.03}\text{O}_{5.985}$  ( $\text{M} = \text{Mg}$  and  $\text{Zn}$ )

	$a$ (Å)	$b$ (Å)	$c$ (Å)
$\text{Nd}_3\text{O}_2\text{GaO}_4$	9.1820(3)	11.5396(3)	5.5748(3)
$\text{Nd}_3\text{Ga}_{0.97}\text{Mg}_{0.03}\text{O}_{5.985}$	9.1842(3)	11.5428(3)	5.5766(3)
$\text{Nd}_3\text{Ga}_{0.97}\text{Zn}_{0.03}\text{O}_{5.985}$	9.1894(3)	11.5480(3)	5.5797(3)

( $r_e^{(\text{IV})} = 0.47 \text{ \AA}$ ) induces a volume increase which, though significant, is limited by the compensating effect of oxygen vacancies.

(b)  $\text{Nd}_3\text{O}_{2-x/2}\square_{x/2}(\text{Ga}_{1-x}\text{M}_x\text{O}_4)$  ( $\text{M} = \text{Mg}, \text{Zn}; x < 0.05$ ). Analysis of XRD data of the sintered samples with  $x \leq 0.05$  indicates that solid solutions are formed up to  $x = 0.03$  only. For  $x = 0.05$ , the cell parameters are nearly identical [within three times the estimated standard deviations (esd's)] to those refined for  $x = 0.03$  (Table 1), and weak extra peaks corresponding to trace amounts of  $\text{Nd}_2\text{O}_3$  were observed on the XRD pattern. Extra peaks corresponding to the MO oxide should be observed, but because we are dealing with trace amounts of an oxide of light elements, they can hardly be detected. Such results indicate that the limit of the solid solution is close to  $x = 0.03$ . Despite its small extent and of the compensating effect of oxygen vacancies, replacement of  $\text{Ga}^{3+}$  by  $\text{Mg}^{2+}$  ( $r_e^{(\text{IV})} = 0.57 \text{ \AA}$ ) or  $\text{Zn}^{2+}$  ( $r_e^{(\text{IV})} = 0.60 \text{ \AA}$ ) does induce a significant volume increase.

(c)  $\text{Nd}_{3(1-x)}\text{M}'_{3x}\text{O}_{2-3x/2}\square_{3x/2}(\text{GaO}_4)$  ( $\text{M}' = \text{Ca}, \text{Sr}; x < 0.05$ ). The XRD data of Ca and Sr substituted samples were analyzed, and the cell parameters were refined. Figure 8 illustrates the evolution of the orthorhombic cell parameters with Ca and Sr content. For  $\text{M}' = \text{Ca}$  and  $x = 0.05$ , weak extra peaks corresponding to trace amounts of  $\alpha\text{-NdCaGaO}_4$ ,<sup>15,16</sup>  $\text{CaO}$  and  $\text{Ga}_2\text{O}_3$  were observed, and the cell

parameters are nearly identical (within three times the esd's) to those refined for  $x = 0.03$ . Similarly, for  $\text{M}' = \text{Sr}$  and  $x = 0.03$ , the cell parameters are nearly identical (within three times the esd's) to those refined for  $x = 0.015$  and weak extra peaks corresponding to trace amounts of  $\text{NdSrGaO}_4$ ,<sup>17</sup>  $\text{SrO}$ , and  $\text{Ga}_2\text{O}_3$  were observed. Such results indicate that the limits of the solid solution are close to  $x = 0.03$  for Ca and 0.015 for Sr substituted phases.

**3.3. Conductivity Measurements.** The ac impedance data were analyzed to determine conductivity values of both bulk and grain boundaries and to study electrode phenomena. Data in the form of Nyquist plots are shown in Figure 9 for  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$  (this sample is a good representative of all samples investigated in the course of this study) at different temperatures. In the low temperature range, impedance diagrams mainly show two overlapping semicircles (Figure 9a). They have been modeled with the use of an equivalent circuit formed with the series combination of two parallel RC circuits. The least-squares fitting leads to capacitances  $C_b \approx 8.7 \pm 0.5 \text{ pF cm}^{-1}$  (the form factor of the sample is  $0.27 \text{ cm}^{-1}$ ) and  $C_{gb} \approx 0.9 \pm 0.3 \text{ nF cm}^{-1}$ , which are in good agreement, respectively, with bulk capacitance (high frequency semicircle) and grain boundary capacitance (intermediate frequency semicircle) usually observed in similar materials such as YSZ ( $C_b \approx 6.5 \text{ pF cm}^{-1}$  and  $C_{gb} \approx 7.3 \text{ nF cm}^{-1}$  in ref 18). As a wide variety of ceramic microstructures occur in practice, it is found that  $C_{gb}$  usually lies in the range  $10^{-11}$  to  $10^{-8} \text{ F cm}^{-1}$ ; that rather high values occur in both  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$  and YSZ<sup>18</sup> is indicative of well-sintered samples with narrow intergranular regions.<sup>19</sup> Such capacitance values were used to model part of the electrical behavior at higher temperature (Figure 9b) where strong overlapping of semicircles makes it difficult to distinguish bulk from grain boundary effects. At lower frequency a third semicircle is observed (see inset of Figure 9b). It was modeled with the use of a third parallel RC circuit in series with those representing bulk and grain boundary contributions. The capacitance of this third semicircle,  $C_{dl} \approx 7 \text{ }\mu\text{F cm}^{-1}$ , is typical of electrical double layer phenomena, but that the data is in the form of a semicircle rather than a vertical spike is associated with electron transfer to and from the oxide ions at the electrode-ceramic interface; that is, the interface response is partially blocking and has a relatively small  $R_{dl}$  resistance. Finally, at the lowest frequencies, a usual inclined spike is observed associated with diffusion-limited processes. It was modeled with a Warburg impedance. In some of the Arrhenius plots given in the next figures, both bulk and total conductivities are displayed in the temperature range where they could be separated accurately.

Although  $\text{Nd}^{3+}$ ,  $\text{Ga}^{3+}$ ,  $\text{Ge}^{4+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Zn}^{2+}$ ,  $\text{Ca}^{2+}$ , and  $\text{Sr}^{2+}$  are not known to be prone to either reduction or oxidation,

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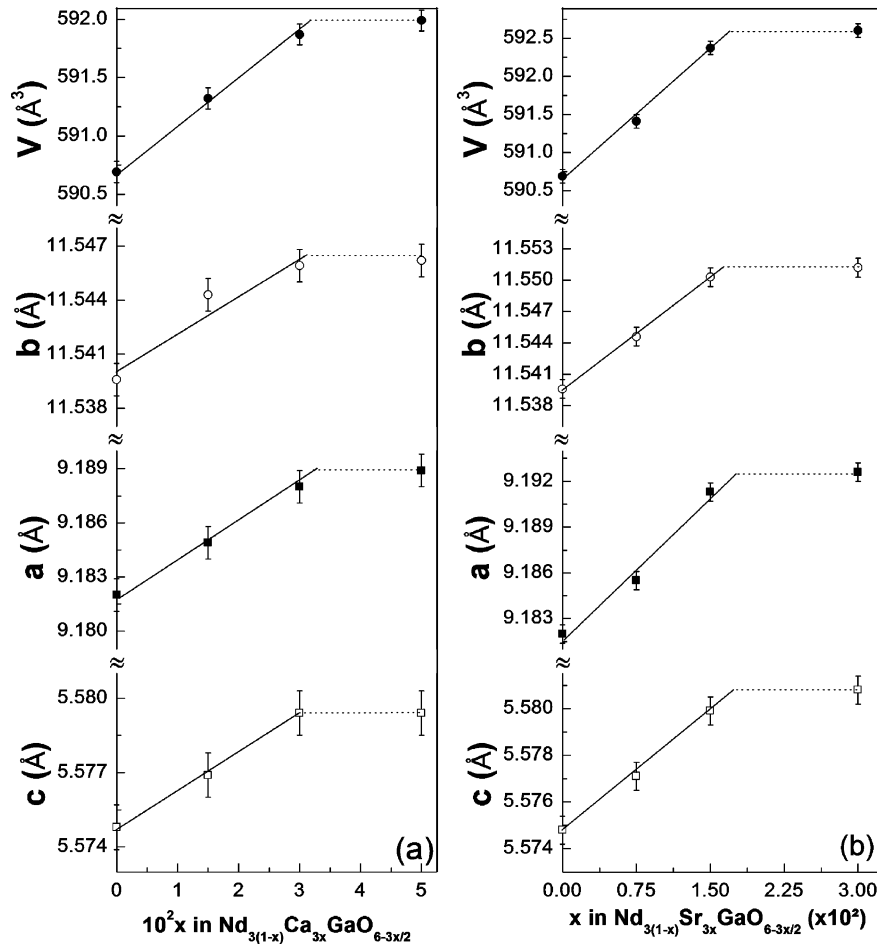


Figure 8. Evolution of cell parameters and cell volume with the  $M'$  content in  $Nd_{3(1-x)}M'_{3x}O_{2-3x/2}\square_{3x/2}(GaO_4)$  compounds: (a)  $M' = Ca$  and (b)  $M' = Sr$ .

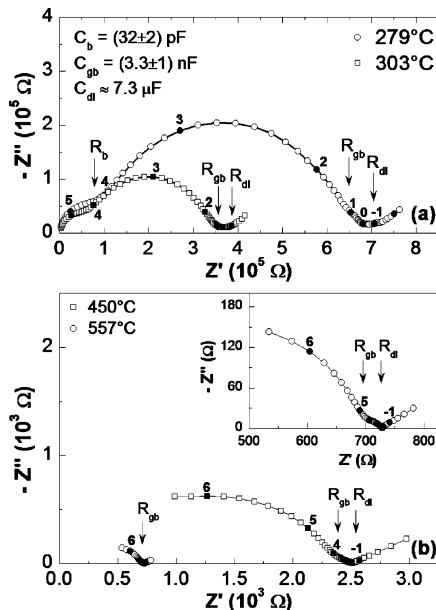


Figure 9. Complex impedance plane plots (figures on the curves denote decades of frequency) for  $Nd_{2.955}Sr_{0.045}GaO_{5.9775}$  at various temperatures (the solid lines are the fittings). An enlarged image of the impedance plot at 557 °C is given in the inset of part b.

all compounds were subjected to conductivity measurements under two reduced oxygen partial pressures ( $10^{-5}$  and  $10^{-20}$  atm). As expected, it was shown that, within experimental error, the conductivities are almost identical to those measured in dry air which indicates that the ionic conductiv-

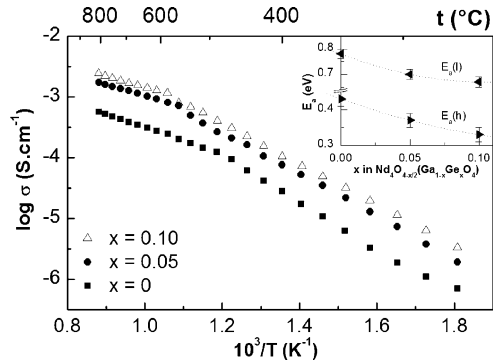
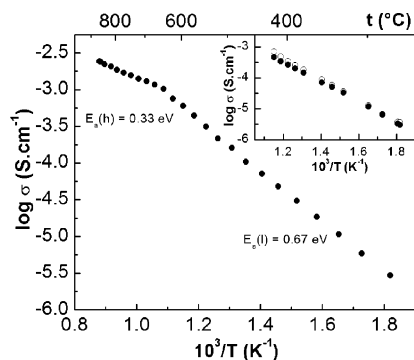


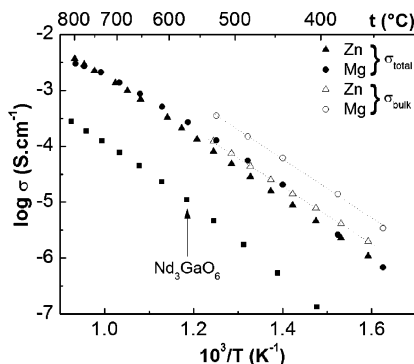
Figure 10. Conductivity data for  $Nd_4O_{4-x/2}\square_{x/2}(Ge_{1-x}Ga_xO_4)$  compounds.

ity is clearly dominant in these materials. Consequently, because the mobility of cationic species mentioned above is very likely negligible, one can conclude that the title materials are pure oxide-ion conductors.

(a)  $Nd_4O_{4-x/2}\square_{x/2}(Ge_{1-x}Ga_xO_4)$  ( $x < 0.125$ ) Compounds. Conductivity results are given in the form of Arrhenius plots in Figure 10. In all cases, the evolution of the conductivity with temperature exhibits two thermally activated regimes with a break at a temperature ranging from  $\sim 450$  °C for  $x = 0$  to  $\sim 550$  °C for  $x = 0.1$ . This feature could be related to a ferroelectric–paraelectric phase transition, that is, a structural change from  $SG Pmc2_1$  to  $SG Pmcm$  (or  $Pmcm$ ).<sup>1</sup> This possible transition is being investigated by dielectric (temperature dependence of the permittivity) and micro-calorimetric measurements. In the low-temperature regime,



**Figure 11.** Arrhenius plots for  $\text{Nd}_4\text{Ge}_{0.9}\text{Ga}_{0.1}\text{O}_{7.95}$  (bulk and total conductivities are represented by open and filled circles, respectively).



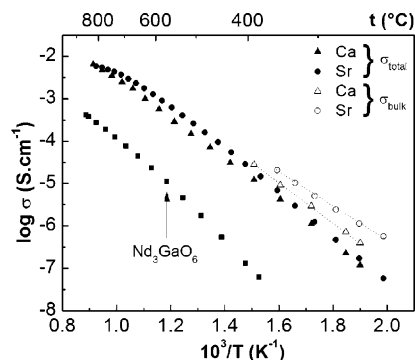
**Figure 12.** Conductivity data for  $\text{Nd}_3\text{O}_2\text{GaO}_4$  and  $\text{Nd}_3\text{Ga}_{0.97}\text{M}_{0.03}\text{O}_{5.985}$  ( $M = \text{Zn}$  and  $\text{Mg}$ ; total and bulk conductivities are represented by filled and open markers, respectively; squares for  $\text{Nd}_3\text{O}_2\text{GaO}_4$ , triangles for  $M = \text{Mg}$ , and circles for  $M = \text{Zn}$ ).

the activation energy  $E_a(l)$  is larger than that at higher temperature  $E_a(h)$  (Figure 10). Both  $E_a(l)$  and  $E_a(h)$  values decrease when  $x$  increases as a probable consequence of a weaker covalent framework. As expected, when  $\text{Ga}^{3+}$  is substituted for  $\text{Ge}^{4+}$ , charge-compensating oxygen vacancies play a beneficial role on the anionic conductivity which increases from  $2.8 \times 10^{-4} \text{ S cm}^{-1}$  for pure  $\text{Nd}_4\text{GeO}_8$  to  $1.9 \times 10^{-3} \text{ S cm}^{-1}$  for  $x = 0.1$ , at  $800^\circ\text{C}$ . For this latter composition, the evolution of both bulk and total conductivities is displayed in Figure 11.

(b)  $\text{Nd}_3\text{O}_{2-x/2}\square_{x/2}(\text{Ga}_{1-x}\text{M}_x\text{O}_4)$  ( $M = \text{Mg}, \text{Zn}; x < 0.05$ ). Figure 12 shows the ion conductivity of  $\text{Nd}_3\text{O}_2\text{GaO}_4$  and  $\text{Nd}_3\text{O}_{1.985}\square_{0.015}(\text{Ga}_{0.97}\text{M}_{0.03}\text{O}_4)$  ( $M = \text{Zn}, \text{Mg}$ ) compounds, as a function of temperature. All curves reflect the expected Arrhenius kind of behavior. The conductivity for pure  $\text{Nd}_3\text{O}_2\text{GaO}_4$  at  $800^\circ\text{C}$  was found to be  $2.7 \times 10^{-4} \text{ S cm}^{-1}$  with an activation energy of 1.2 eV.

Despite limited substitution rates of  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  for  $\text{Ga}^{3+}$  in  $\text{Nd}_3\text{O}_2\text{GaO}_4$  (as demonstrated by XRD analysis) a significant improvement in the ionic conductivity was observed. The ionic conductivity for  $\text{Nd}_3\text{O}_2\text{GaO}_4$  doped with 3%  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  was found to be  $0.5 \times 10^{-2}$  and  $0.4 \times 10^{-2} \text{ S cm}^{-1}$  at  $800^\circ\text{C}$ , with activation energies of 1.08 and 1.2 eV, respectively.

The difference between bulk and total conductivities in the case of the Mg-substituted compound is larger than for the Zn-doped material (Figure 12), although both samples had almost the same density. This result is likely related to the smaller grain size of the Mg- compared to the Zn-doped sample, thus, leading to a larger grain boundary effect.



**Figure 13.** Conductivity data for  $\text{Nd}_3\text{O}_2\text{GaO}_4$ ,  $\text{Nd}_{2.91}\text{Ca}_{0.09}\text{GaO}_{5.955}$ , and  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$  (total and bulk conductivities are represented by filled and open markers, respectively; squares for  $\text{Nd}_3\text{O}_2\text{GaO}_4$ , triangles for  $\text{Nd}_{2.91}\text{Ca}_{0.09}\text{GaO}_{5.955}$ , and circles for  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$ ).

(c)  $\text{Nd}_{3(1-x)}\text{M}'_{3x}\text{O}_{2-3x/2}\square_{3x/2}(\text{GaO}_4)$  ( $M' = \text{Ca}, \text{Sr}; x < 0.05$ ). The oxygen ion conductivity of  $\text{Nd}_3\text{O}_2\text{GaO}_4$ ,  $\text{Nd}_{2.91}\text{Ca}_{0.09}\text{GaO}_{5.955}$ , and  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$  compounds, as a function of temperature, is shown in Figure 13. As in the case of  $\text{Zn}^{2+}$  and  $\text{Mg}^{2+}$  substituted compounds, it can be seen that the creation of a small rate of oxygen vacancies in the  $\text{Nd}_3\text{O}_2\text{GaO}_4$  structure, concomitant with substitutions of  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  for  $\text{Nd}^{3+}$ , induces a significant increase of the anionic conductivity which reaches  $0.6 \times 10^{-2}$  and  $0.7 \times 10^{-2} \text{ S cm}^{-1}$ , at  $800^\circ\text{C}$ , for  $\text{Nd}_{2.91}\text{Ca}_{0.09}\text{GaO}_{5.955}$  and  $\text{Nd}_{2.955}\text{Sr}_{0.045}\text{GaO}_{5.9775}$ , respectively. Activation energies for these Ca and Sr substituted compounds, 0.97 and 1.06 eV, respectively, are, as expected, rather close to those of other  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials.

#### 4. Conclusion

A novel wet-chemical process based on EDTA–nitrate combustion has been developed, which has a potential to produce phase-pure, ultrafine, well-sinterable powders of  $\text{Nd}_4\text{O}_4\text{GeO}_4$ - and  $\text{Nd}_3\text{O}_2\text{GaO}_4$ -based materials. They have been characterized by XRD on powder samples. It was found that cation substitution with lower valent cations to form charge-compensating oxygen vacancies was possible only at the  $\text{Ge}^{4+}$  site of  $\text{Nd}_4\text{O}_4\text{GeO}_4$  and at both cation sites of  $\text{Nd}_3\text{O}_2\text{GaO}_4$ . However, it was observed that both structures are not very prone to accept large rates of oxygen vacancies.  $\text{Nd}_4\text{Ge}_{1-x}\text{Ga}_x\text{O}_{8-x/2}$  is formed up to  $x = 0.10$ ,  $\text{Nd}_3\text{Ga}_{1-x}\text{M}_x\text{O}_{6-x/2}$  ( $M = \text{Zn}, \text{Mg}$ ) up to  $x = 0.03$ , and  $\text{Nd}_{3(1-x)}\text{M}'_{3x}\text{GaO}_{6-3x/2}$  up to  $x = 0.03$  and 0.015 for  $M' = \text{Ca}$  and  $\text{Sr}$ , respectively. Despite these small substitution rates, significant improvements of the anionic conductivity are observed for all substituted compounds.

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